

A SIMPLE MOLAR FLOW MODELING AND SIMULATION OF CATALYTIC BEDS IN CLAUS PROCESS

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Abstract

The Claus process has been known and used in the industry for over 100 years. It involves thermal oxidation of hydrogen sulfide and its reaction with sulfur dioxide to form sulfur and water vapor. This process is equilibrium-limited and usually achieves efficiencies in the range of 94-97%, which have been regarded as acceptable in the past years. First bed operates at the temperature of 573 K, second and third beds operate at 523K and 473K. Outlet of each bed enters the condenser. Operating temperature of each condenser is about 413K which sulfur condenses in them. In this study catalytic bed process of sulfur recovery unit has been mathematically modeled and by MATLAB software simulated, and then output conditions of compounds has been calculated.

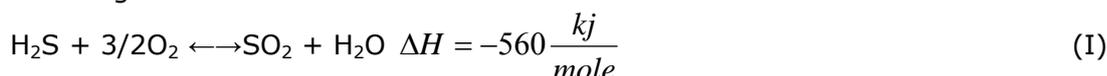
Key words: Sulfur recovery; Claus process; Catalytic beds; Modeling; Simulation.

1. Introduction

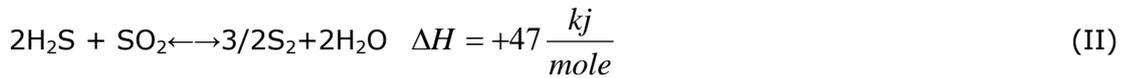
Claus process which is used nowadays is a modern process precedes the one Pioneered in 1883 based on the reaction of H₂S over a catalyst base with air (oxygen) in shape of sulfur and water [1]. Sulfur recovery refers to the conversion of hydrogen sulfide (H₂S) to elemental sulfur. Hydrogen sulfide is a byproduct of processing natural gas and refining high-sulfur crude oils [2,3]. The most common conversion method used is the Claus process. Approximately 90 to 95 percent of recovered sulfur is produced by the Claus process. The Claus process typically recovers 95 to 97 percent of the hydrogen sulfide feed stream. Clause process briefly described bellow [4].

Process Description

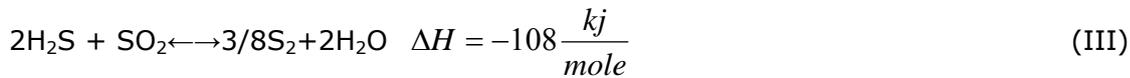
Hydrogen sulfide, a byproduct of crude oil and natural gas processing, is recovered and converted to elemental sulfur by the Claus process. The process consists of multistage catalytic oxidation of hydrogen sulfide; each catalytic stage consists of a gas reheater, a catalyst chamber, and a condenser. The Claus process involves burning one-third of the H₂S with air in a reactor furnace to form Sulfur dioxide (SO₂) according to the following reaction:



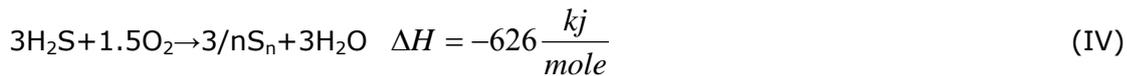
The furnace normally operates at combustion chamber temperatures ranging from 980 to 1540°C (1800 to 2800°F) with pressures rarely higher than 70 kilopascals (kPa). Before entering a sulfur condenser, hot gas from the combustion chamber is quenched in a waste heat boiler that generates high to medium pressure steam. About 80 percent of the heat released could be recovered as useful energy. Approximately 65 to 70 percent of the sulfur is recovered. The cooled gases exiting the condenser are then sent to the catalyst beds. The remaining uncombusted two-thirds of the hydrogen sulfide undergoes Claus reaction (reacts with SO₂) to form elemental sulfur as follows:



The remaining H_2S , from the Claus furnace, is reacted with the SO_2 at lower temperatures (about 470-620 K) over an alumina- or titanium dioxide-based catalyst to make more sulfur:



On average, about 70% of H_2S and SO_2 will react via reaction (III). Note that in the catalytic stage mostly S_8 is produced, which is an exothermic reaction whereas in the thermal stage S_2 is the major product and the reaction is endothermic. Other allotropes of sulfur may also be present in smaller quantities. The overall reaction for the entire process is:



A typical arrangement for the Claus sulfur recovery process is shown in Fig. 1.

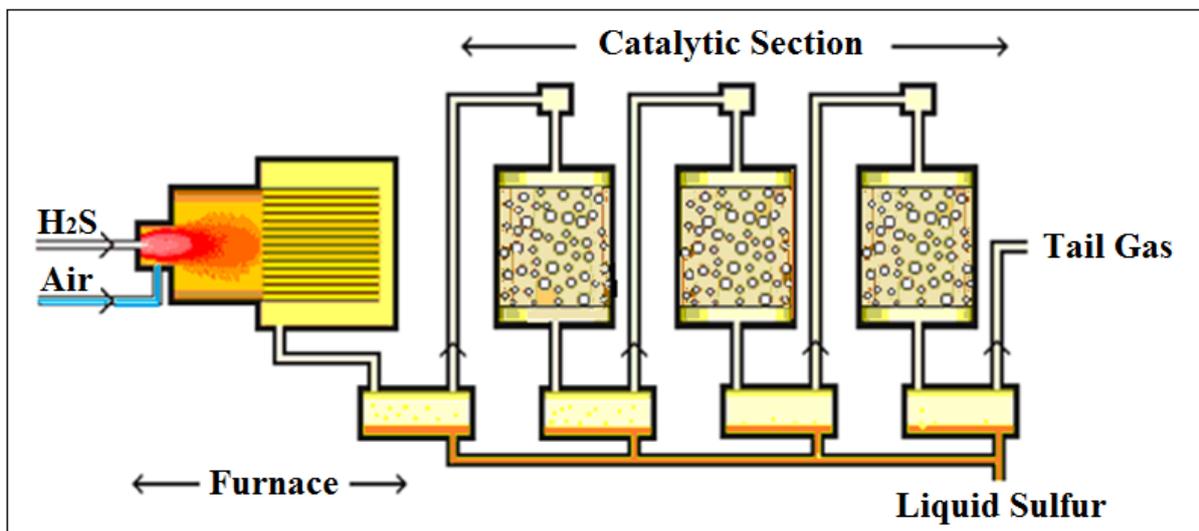


Fig. 1. Typical arrangement of a Claus unit [4]

Because this reaction represents an equilibrium chemical reaction, it is not possible for a Claus plant to convert all the incoming sulfur compounds to elemental sulfur. Therefore, 2 or more stages are used in series to recover the sulfur. Each catalytic stage can recover half to two-thirds of the incoming sulfur. The number of catalytic stages depends upon the level of conversion desired. It is estimated that 95 to 97 percent overall recoveries can be achieved depending on the number of catalytic reaction stages and the type of reheating method used.

High-pressure steam (40 atm) is generated in the boiler stage and low-pressure steam (3-4 atm) is produced in the condensers. A total of two to four catalytic stages are typically used in order to maximize efficiency.

The Claus process is equilibrium-limited. In the furnace stage the SO_2 produced from the combustion process (reaction I) recombines with H_2S in an endothermic reaction to form S_2 (reaction II). Adequate residence time has to be provided in order to allow this reaction, responsible for 60-70% of sulfur conversion, to reach equilibrium. Since the main Claus reaction III is exothermic, this stage calls for the use of low temperatures in order to shift the equilibrium constant towards higher product yields. The low temperatures, however, lead to decreased reaction rates, hence the need for a catalyst. The law of mass action for the Claus reaction is as follows:

$$K_p(T) = \frac{P_{\text{H}_2\text{O}}^2 \times P_{\text{S}_8}^{\frac{3}{8}}}{P_{\text{H}_2\text{S}}^2 \times P_{\text{SO}_2}} \quad (1)$$

Where, $K_p(T)$ is the chemical equilibrium constant and $P_{\text{H}_2\text{O}}$, P_{S_8} are partial pressures of the products and $P_{\text{H}_2\text{S}}$, P_{SO_2} are partial pressures of the reactants. This equation

illustrates the nature of equilibrium limitations involved in the Claus process; decreasing the process temperature can increase the equilibrium constant and thus increase conversion, but the lower

Limit of this temperature and hence the upper limit of equilibrium conversion is set by the condensation temperature of sulfur [1-10].

2. Modeling of Catalytic Beds

Modeling of this process consists of three parts which are mass balance and condenser formulation. In a case of molar flow and energy balance we used the rate formula of reaction II. Kinetic reaction of (II) in the temperature of 200 and 300(°C) is as follow [9]. Because all the three catalytic beds operate at same temperature range this formula seems to be correct:

$$r = K_1(T)P_{H_2S}P_{SO_2}^{0.25} - K_2(T)P_{H_2O} \quad (2)$$

In the above equation if we put $P_i = C_iRT$ then we have:

$$r = K_1(T)(RT)^{1.25}C_{H_2S}C_{SO_2}^{0.25} - K_2(T)(RT)C_{H_2O} \quad (3)$$

K_1 and K_2 are defined as bellow:

$$K_1 = K_{10} \exp\left(-\frac{E_1}{RT}\right) \quad (4)$$

$$K_2 = K_{20} \exp\left(-\frac{E_2}{RT}\right) \quad (5)$$

K_1 and K_2 are activation energy of reaction in the forward and reverse side. The values of K_{10} , K_{20} , E_1 and E_2 are as bellow:

$$K_{10} = 15762 \frac{\text{mole}}{\text{m}^3 \cdot \text{s}}, \quad K_{20} = 506 \frac{\text{mole}}{\text{m}^3 \cdot \text{s}}, \quad E_1 = 49.4 \frac{\text{kJ}}{\text{mole}}, \quad E_2 = 89.3 \frac{\text{kJ}}{\text{mole}}$$

2.1. Molar Flow Balance

We consider catalytic bed as Fig 2; by choosing an element on the bed we write molar flow balance equations:

$$\text{Input} - \text{Output} + \text{generation} - \text{consumption} = 0 \quad (6)$$

$$(uC_i s)_z - (uC_i s)_{z+dz} + s \frac{dn_i}{v dt} = 0 \quad (7)$$

$$u \frac{dC_i}{dz} + Kf(C_i) = 0 \quad (8)$$

$$u \frac{dC_i}{dz} + r_i = 0 \quad (9)$$

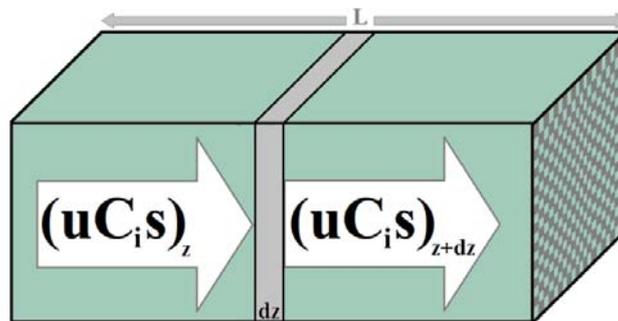


Fig. 2. Sample modeled catalytic bed for mass balance

In above equation i is related to each element of reaction. For solving the equations (7) to (9), we need the rate of reaction of each component. We use rate of reaction of H_2S as a basis for our calculations. Rate of each component in the reaction has a relation with stoichiometric factor of that component in the reaction, so we can calculate the rate of each component in the reaction with respect to rate of H_2S then by substitution of Eq. (12) in the equation of Eq. (7) to (9) we solve the problem.

$$\frac{-r(H_2S)}{2} = -r(SO_2) = \frac{2r(S_2)}{3} = \frac{r(H_2O)}{2} \quad (10)$$

2. 2. Condenser Formulation

Gas composition of inlet gas to the condenser contains a large amount of sulfur; because the condenser temperature is about 140°C so the produced sulfur will be condensed and separated. The most important point in sulfur recovery in the catalytic bed is that all the sulfur is not totally separated in each bed, and a portion of the sulfur will enter the next bed, so the condensed sulfur in second and third bed is equal to the sum of produced sulfur of that bed and amount of sulfur that is transferred from the previous bed. Amount of sulfur that is remain in gaseous phase in each condenser and entered to the next bed is calculated from bellow relations:

$$x_s P_s^* = y_s P_t \quad (11)$$

Because the liquid phase in the condenser only contains sulfur so $x_s = 1$. P_s^* is the saturation pressure of the sulfur and P_t is operating pressure.

$$y_s = \frac{P_s^*}{P_t} \quad (12)$$

$$Y_s = \frac{y_s}{1 - y_s} \quad (13)$$

$$G_s = G(1 - y_s) \quad (14)$$

$G_s Y_s$ is the amount of condensed sulfur that is entered to the next bed.

3. Simulation of Process

Simulation of this process has been done by using MATLAB software. All the operating condition and all the physical and chemical characteristic of the component have been considered. Physical properties are used as a function of temperature. Amount of inlet sulfur entered to the first bed assumed to be 0,1 kmol/hr. We assume this amount of sulfur is from the furnace.

4. Results

Results of simulation whit respect to inlet condition of table1 are as follow. Also, the length of catalytic bed assumed to be 2m ; this length is divided to 100 parts.

Table 1. Inlet value of each component in the first bed

Component	H ₂ S	SO ₂	H ₂ O	S ₂
Inlet Value (kmol/hr)	2	1	0	0.02

Figures 3 to 7 are obtained by solving molar flow balance equation. As it is clear the composition of H₂O and S₂ will be increased, and the composition of H₂S and SO₂ will be decreased. Because the variation of compositions in second and third beds are less sensible, variation of compositions of S₂, H₂S, SO₂ and H₂O are shown separately. Results of running our program for molar flow balance are shown in table 2. By considering figure 3 to 7, the concentration of H₂O and S₂ increase along the bed and concentration of H₂S and SO₂ decrease along the bed.

Table 2. Flow rate of components in each bed

Inlet /Outlet Flow Rate of the Beds (kmol/hr)	H ₂ O	S ₂	SO ₂	H ₂ S
Inlet Flow rate to the First bed	0	0.02	1	2
Outlet Flow rate from the First bed	1.8519	1.3889	0.074	0.1481
Inlet Flow rate to the Second bed	1.8519	9.707e-5	0.074	0.1481
Outlet Flow rate from the Second bed	1.8809	0.0219	0.0595	0.1191
Inlet Flow rate to the Third bed	1.8809	6.711e-5	0.0595	0.1191
Outlet Flow rate from the Third bed	1.8866	0.0043	0.0567	0.1134

In each bed, for simplifying the molar flow balance and achieve the rapid estimation of condensed sulfur, accumulation term in molar flow equation was assume zero. By the way the results from simulation are logical and can be used for other similar process.

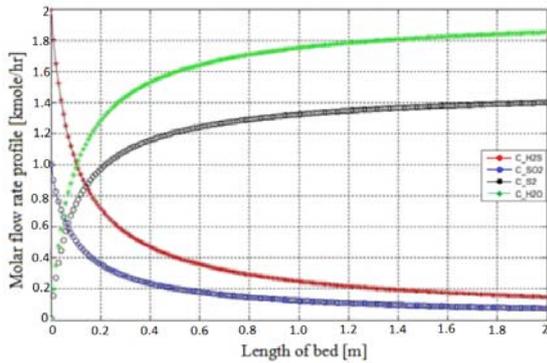


Fig. 3. Molar flow rate variation of H₂O, S₂, SO₂, and H₂S in the first catalytic bed

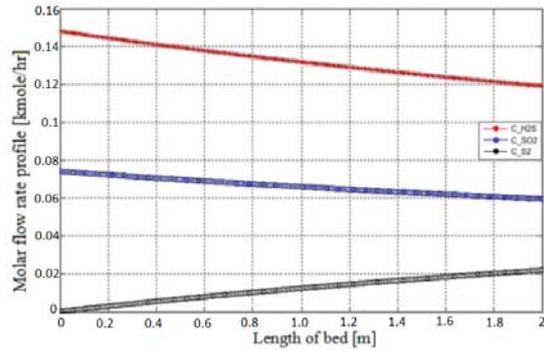


Fig. 4. Molar flow rate variation of S₂, SO₂, and H₂S in the second catalytic bed

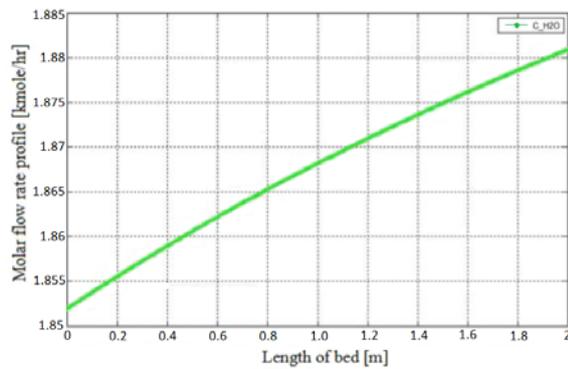


Fig. 5. Molar flow rate variation of H₂O in second catalytic bed

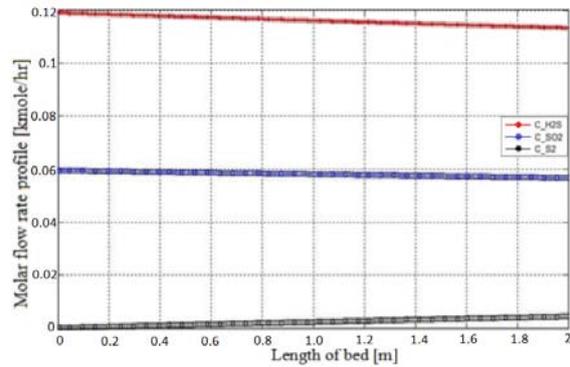


Fig. 6. Molar flow rate variation of H₂S, SO₂ and S₂ in the third catalytic bed

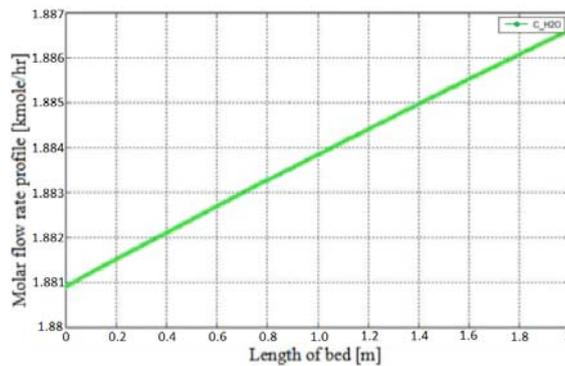


Fig. 7. Molar flow rate variation of H₂O in the third catalytic bed

5. Conclusion

This research was carried out in a gas refinery plant, in this study, sulfur separation process via catalytic bed modeled and simulated. Modeling has been done with the basis of molar flow balance relations. Inlet flow rate to the first bed has been shown in the table 1. The length of catalytic bed assumed to be 2m, this length divided to 100 parts, and in each point of division the molar flow equation have been solved, so molar flow rate of each component in each bed has been calculated. With a simple calculation sulfur mass balance can be shown, so:

$$\{\text{Sulfur (Furnace)} + \text{Sulfur (SO}_2\text{)} + \text{Sulfur (H}_2\text{S)}\} = \{\text{Sulfur (out put)} + \text{Sulfur (Condensed)}\}$$

By solving above relation it is shown that inlet and outlet sulfur is about 3.02 kmol/hr. This amount of sulfur is equal to separation of about 1200 kg/day sulfur in a sour gas sulfur recovery unit. By this method we can define outlet condition of catalytic bed products.

Nomenclatures

ΔH	Reaction Enthalpy Difference (kJ/mol)	v	Volume of the bed (m^3)
T	Temperature (K)	n	Amount of material (kmol)
P	Pressure (Pa)	r	Rate of reaction ($(kmole/m^3s)$)
C_i	Component's Concentration ($kmol/m^3$)	R	Gas constant ($pa.m^3/kmole.K$)
E_1	Activation Energy; Forward reaction(kj/mol)	p_s^*	Sulfur saturation pressure (pa)
E_2	Activation Energy; Reverse reaction(kj/mol)	p_t	Operating pressure (pa)
u	Average flow velocity in bed (m/s)	x_s	Percent of sulfur in liquid phase
s	Cross sectional area of bed (Catalyst) (m^2)	y_s	Percent of sulfur in gas phase
t	Time (sec)	G	Gas phase flow rate in condenser (kmole/hr)

Acknowledgments

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